# **Risks which Caused by Obesity on the Spine**

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**ABSTRACT:** The objective of this work is to study the effect of obesity on the intervertebral discs and provide system analysis of the spine between multiple configurations of people, and know the risks due to this eccentric load (Big Belly). The results show in all three previous loadings (obese people), the distributions of stress and strain are high in both D1 and D10 intervertebral discs. This shows that the distance between the point of load application and the spine axis has an important role in solicitation increasing and therefore its deformation: as main conclusion is that the concentration of the mass of stomach fat is a risk factor that leads to pain problems, deformation and herniated disc.

**Keywords:** Obese; Lumbar-Thoracic; Intervertebral Discs; Finite Element; Biomechanics; Von Mises Stress-Strain; Disc Degeneration.

# I. INTRODUCTION

The prediction of the mechanical behavior of the spine system is one of the major problems of biomechanics [1]. A better understanding of moving mechanisms of spine under different loads and stress distribution in this system is of fundamental importance in the advancement of technologies in the areas of spinal restorations inter vertebral prostheses, and ortho- ontology [2].

The spine or rachis consists of a movable column of 24 free vertebrae and a fixed column formed of fused vertebrae: the sacrum and coccyx **"Figure 1"**; it is the fixing strut of many essential muscles in the posture and locomotion and protects the spinal cord located in the vertebral canal; it supports the head and transmits the weight of the body to the hip joints; with a length of about 70 cm in men (60 cm in women), its reduction may reach 2 cm when standing **[3]**.

The degeneration of the lumbar discs is definitely linked to BMI, overweight and obesity is associated with a higher risk of spine problems. The term obesity is defined as an eccentric load "**Figure 2**"; the load is represented by the mass of the belly (P1). The MRI study [4], alerts of this overweight effect in the development of degenerative disc disease, back pain and then herniated disc "**Figure 3**".

In this work, the simulation of the disc degeneration, based on a finite element model of the spine depending on the mechanical properties were established; the boundary condition has been applied in the frontal plane to define restriction on movements of translation and rotation of the spine. We propose in this work to draw up a comprehensive study of stresses and deformations in the spinal discs distributions based on supported loads. The results show that the level of degeneration increased in all intervertebral discs but concentrated in the two disks D1 and D10.



Figure 1. Anatomy of the lumbar spine [5].



Figure 2. Constitution spine (obese person) at the disc depending on its condition.

Figure 3 shows two vertebrae of the spinal column with an intervertebral disc under the effect of a compound loading (compression P + bending moment P1). The compressive load P creates an internal pressure in the nucleus, this pressure will there after generate the disc degeneration or degenerative disc disease "Figure 4", as regards the forward flexion P1, if the load of the stomach increases, automatically distance between the point of load application and the axis of the spinal column increases, we see that the posterior portion of the annulus fibrosis is tensioned and the other front portion is compressed, that is to say the nucleus pulposus burst back (posterior compression), this compression produced by disc protrusion comes into contact with a nerve root called herniated disc.



Figure 3. The intervertebral disc with (a) bending (b) compression [6].



Figure 4. Load distribution at the disc D1 according to his state [7]. II. MATERIAL AND METHODS

The objective of this work is to provide an analysis between a geometric configuration of the spine system, to find the effect of eccentric loads on the latter and mainly on the inter vertebral discs by analyzing the stress distribution in this system using a 3D numerical simulation, based on the principles of the finite element method. The analysis of biomechanical problems includes several steps. The first is to study the form to define the geometrical configuration of the object, which allows the reconstitution of the vertebra, the ligament and bone using CAD programs. The result is a 3D geometric model including these three components will then be prepared for use in finite element analyzes for the study of stresses and deformations distribution in the system.

#### The steps for the execution of the 3D vertebra model "Figure 5" are as follow:

**a**) Draw cortical bone that is the upper hinge and the lower hinge, then make the smoothing process; this gives a solid body called the vertebral body.

**b**) Secondly, draw the posterior arch (blade with the pedicle) with the spinous process.

c) Finally we draw the transverse process.



Figure 5. Lumbar vertebras.

The simulation of the disc degeneration is based on a finite element model of the healthy spine. **Figure 6** shows a spine model, this consists of five lumbar vertebrae (L1, L2, L3, L4 and L5) plus the sacrum, twelve thoracic vertebrae (TH1, TH2, TH3, TH4, TH5, TH6, TH7, TH8, TH9, TH10, TH11, TH12) and 17 inter vertebral discs between (S1-L5, L5-L4, L4-L3, L3-L2, L2-L1, L1-TH12 TH12-TH11, TH11, TH10, TH10-TH9, TH9-TH8, TH8-TH7, TH7-TH6, TH6-TH5, TH5-TH4, TH3-TH4, TH3-TH2 TH2-TH1) and various ligaments thoracic lumbar spine (anterior longitudinal ligament, posterior longitudinal ligament, ligament interspinous, ligament supraspinatus, yellow ligament and capsular ligament).



Figure 6. Spine studied.

#### (a): Lateral (left) view. (b): dorsal view. (c): front view. (d): lateral (right) view

In static loading conditions, the model of the reconstructed spine is used in an analysis for studying the role of the inter vertebral discs and the stress distribution in these disks as well as its supporting structures. The spine is reconstructed in 3D to study the system dimensions (IVD - ligament-bone) **"Figure 7"**.



Figure .7 Vertebra and sacrum dimensions.

In order to define the boundary conditions, restriction on movements of translation and rotation of the spine has been applied in the lower plane, and defined as having zero displacements.

# Several charges in the anterior direction were applied as follows:

- The application of the load on the upper side of the thoracic vertebra TH1.
- The fixed part applied to the body of the sacrum.
- The interfaces between the different components of the system of the spine, the cortical bone, the inter vertebral disk and ligament are treated as perfectly bonded interfaces **"Figure 8"**.

Figure 9 shows an isometric view of an explored assembly of the spine and each component of the spine system is denoted by letters.







Figure .9 Assemblies in isometric perspective.

# Abbreviations

**D**<sub>1</sub>: intervertebral disk upstairs one.

 $N_1$ : nucleus in the intervertebral disc upstairs one.

**D**<sub>10</sub>: intervertebral disk upstairs ten.

 $N_{10}$ : nucleus in the intervertebral disc upstairs ten.

 $L_4$ : lumbar vertebra is on level four.

**D**<sub>4</sub>: intervertebral disk upstairs four.

 $N_4\!\!:$  nucleus in the intervertebral disc upstairs four.

MRI: magnetic resonance imaging.

FEM: Finite Element Method.

## IVD: inter vertebral disc.

The selection of constitutive equations of the vertebral bone is defined as the part of the bone which carries the inter vertebral disc, composed of cortical bone, cancellous bone, the posterior arch, with a Young's modulus of about 12000 MPa. It is well known that cortical bone has better load capacity than the cancellous bone. Cortical bone is considered as an isotropic material, and homogeneous linear elastic.

Authors	σ <sub>r</sub> (MPa)
BROWN (axial direction)	1.4
GALANTE (horizontal direction)	$3.5 \pm 0.3$
GALANTE (fiber direction)	$10.7 \pm 0.9$
WU	3.7

Table 1. Mechanical characteristics of disc tissue [9].

Table 1 shows the tensile strength of the structure annulus fibrosis according to different authors. These materials are in herently anisotropic and non-linear elastic. The behavior of inter-transverse ligament and inter-spinous ligament is nonlinear viscoelastic as in previous studies [8]; a linear elastic model is chosen to represent this behavior. Ansys Workbench software was used for analyzing this geometry and generate the most suitable mesh. For the studied behavior, we used tetrahedral elements, type Solid187 conforming to defined parametric surfaces "Figure 10". It is necessary to mesh the components of the spine with small and confused elements to ensure optimum accuracy of the results of stresses and strains in the inter vertebral discs. The material properties of the spine components were selected after a careful review of the published literature "Table 2"; it was considered appropriate to define the cortical and cancellous bone as homogeneous and isotropic. The magnitudes of 12000 MPa and 100 MPa (cortical and cancellous, respectively) were observed in all studies by various researchers. Since physiologically the nucleus is fluid filled, the elements were assigned low stiffness values (1MPa) and near incompressibility properties (Poisson's ratio of 0.499). Biologically, the annulus fibrosus is comprised of layers of collagen fibers, which attributes to its non-homogenous characteristics. However, due to limitations in modeling abilities, the annulus was defined as a homogenous

structure with a magnitude of 4.2 MPa. This was based on the modulus of the ground substance (4.2 MPa) and the collagen fibers reported in the literature, taking into account the volume fraction of each component.



Figure 10. Spine 3D finite element modeling (Ansys14.5 software).

## **Table 2.** Material Properties Specified in the Model.

The complete model of the spine **"Figure 10"** was realized by the *SOLIDWORKS SOFTWARE Version* 2014 And Was Then Transferred To The Software Calculates Each Element Ends *Ansys 14.5 Workbenche* Generated The Default Mesh Then Generated Linear Global Custom Mesh Tetrahedra 10 Nodes Conform To Surface. The three views of spine model with condensed mesh are shown in **"Figure 10"**. All element and node numbers are specified in **"Table 3"**.

**Figure 10** shows a complete model that consists of 11762783 elements and 17150901 nodes. Cortical bone contains (3585646 element and 5132199 nodes), cancellous bone contains (2496448 element 3471929 nodes). The posterior arch was modeled with tetrahedral elements to 10 nodes contains (2377091 element, 3440842 nodes), the nucleus pulposus in the annulus fibrosus were modeled with tetrahedral type elements 10 nodes (504657 element 717 205 nodes), the annulus fibrosus were modeled with elements of type tetrahedral to 10 nodes (1434546 element , 2059247 nodes). The gelatinous cartilage modeled with a tetrahedral element to 10 nodes (912759 elements, 1431242 nodes). Finally the different types of ligaments generated by a tetrahedral mesh to 10 nodes **"Table 3"**.

Material	Young modulus	Poisson	REFERENCES
	(MPa)	coefficient	
Cortical Bone	12000	0.3	[10,12,13,14,15,16,17,18,19,20
			,21,26,35,37,38,39,40,42,43]
Cancellous Bone	100	0.2	[10,13,14,16,17,18,20,21,23,24
			,25,26,35,37,38.39,40,42,43]
Posterior Bone	3500	0.25	[12,13,14,17,18,20,21,23,26,27
			,36,37,38,39]
Cartilage Endplates	12000	0.3	[20,22,24,28]
Annulus Ground Substance	4.2	0.45	[10,13,16,18,19,20,21,22,24,26
			,30,31,34,35,36,37,38,39,42,43
			]
Nucleus Pulposus	1	0.499	[11,13,14,15,17,19,20,26,29,32
			,33,34,35,36,37,38,42,43]
Anterior Longitudinal	20	0.3	[13,14,16,17,18,36,37,40,41]
Ligament			
Posterior Longitudinal	20	0.3	[13,14,16,17,36,37,40,41]
Ligament			
Ligamentum Flavum	19.50	0.3	[13, 14, 16, 17, 36, 37, 40, 41]
Intertransverse Ligament	58.7	0.3	[13, 14, 16, 17, 36, 37, 40, 41]
Inter-Spinous Ligament	11.6	0.3	[13,14,16,17,36,37,40,41]
Supra-Spinous Ligament	15	0.3	[13,14,16,17,36,37,40,41]
Capsular Ligament	32.9	0.3	[13, 14, 16, 17, 36, 37, 40, 41]

COMPONENT	NODES	ELEMENTS	Thickness
Cortical Bone	5132199	3585646	1mm
Cancellous Bone	3471929	2496448	1mm
Posterior Bone	3440842	2377091	1mm
Cartilage endplates	1431242	912759	1mm
Annulus Ground Substance	2059247	1434546	1mm
Nucleus Pulposus	717205	504657	1mm
Anterior Longitudinal Ligament	227078	128365	1mm
Posterior Longitudinal Ligament	158748	92426	1mm
Ligamentum Flavum	30226	13447	1mm
Transverse Ligament	285328	131648	1mm
Inter-Spinous Ligament	28968	13158	1mm
Supra-Spinous Ligament	17833	8279	1mm
Capsular ligament	51816	24072	1mm
TOTAL	17150901	11762783	1mm

 Table 3. Element and node numbers in the column vertebral system components.



Figure 11. Mechanical model of the spine anterior load (normal person).



Figure 12. Mechanical model of the spine [anterior load (fat person).

The diagram in **"Figure 11"** shows a normal person standing with a specific weight of 80 kg, the total mass (belly) is 13.25 kg representing the weight P1; the pressure load P is the mass of the top portion of the person's body (hands, forearms, arms, head) divided by the area of the thoracic vertebra TH1.

The length of the spine (thoracic + lumbar) is 72 cm and the distance between the specific weights of the belly which is the point of application of the load and the axis of the vertebral column (20cm). For boundary conditions, the sacrum is fixed. (Embedding the sacrum **"Figure 12"**.

We propose in this section to draw up a detailed study of Von Mises distributions constraints and deformations in the intervertebral discs as a function of supported loads.

**Figure 12** shows three people in standing position, with respective specific bellies weight P1 (16.56Kg, 19.88kg, 24.85kg).

The distance between the center of gravity of the belly and the axis of the vertebral column is between  $(30 \text{cm} \div 50 \text{cm})$ , the pressure load P is applied on the thoracic vertebra TH1.

To define the boundary conditions, restriction on movements of translation and rotation of the spine has been applied including frontal plane and defined as having zero displacements on the sacrum see **"Figure 12"**.

Consider the example of an anterior load (obese person), the colors represent the Von Mises stresses experienced by 17 intervertebral discs, blue represents the minimum stress and the red represents the maximum stress.

#### **III. RESULTS**

Figure 13 shows clearly that the anterior load affects the disk D1 and D10 is the two most sought discs compared to other drives in the thoracic lumbar spine.

A load applied to the upper surface of the TH1 thoracic vertebra of the spinal column causes a high concentration of maximum Von Mises stresses in the anterior portion of the two discs D1 and D10 (red section) this is mentioned in **"Figure 15"**.

Moreover, the Von Mises stresses are minimal at the posterior part of the two intervertebral discs D1, D10 (blue contour) see "Figure 15".

**Figure 14** shows the Von Mises strain histogram in the inter vertebral discs for a normal person load 13.25 kg. We note that the Von Mises deformation values are highest in the two discs D1, D10 (2784, 2377) outline in red; this is mentioned in **Figure 16**.



Figure 13. Histogram of the Von Mises stress in the IVD for a load of 13.25 kg.



Figure 14. Histogram of the Von Mises strains in the IVD for a load of 13.25 kg.



Figure 15. Von Mises stresses Distribution in the discs D1 and D10 for a load of 13.25 kg.

Figure 16. Von Mises strains Distribution in the discs D1 and D10 for a load of 13.25 kg.







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Figure 18. Histogram of the Von Mises stress and strains in the IVD for a Diffrent load. (a): 16.56 kg. (b): 19.88 kg. (c): 24.85 kg

Consider the example of an anterior load (obese person), the colors represent the Von Mises stresses experienced by 17 intervertebral discs, blue represents the minimum stress and the red represents the maximum stress. **Figure 17** shows the role of the intervertebral discs in the stress absorbing. Their distribution in the spine tends to be concentrated in the disc D1 on both sides, for the front side, a tracted portion to a maximum value of 15.216 MPa and the other has a minimum value of 0,035 MPa **"Figure 18"**.



Figure 19. Histogram of the Von Mises stress and strains in the IVD for a Different loads.



Figure .20 Distribution of the Von Mises stress and strains in the Discs D1 for load 24.85 kg.

## V. DISCUSSION

We see in **Figure 18** and **Figure 19** Von Mises stresses reached a maximum value concentrated in the two discs D1, D10 which are equal to 15.21 MPa, 13.96 MPa for the first person, 19.454 MPa, 18.217 MPa for the second person and 29.595 MPa, 27.862MPa for the third person who is located in the anterior portion of the disc (red part).

Regarding the deformations Von Mises, we notice that the values are greatest in the two intervertebral discs D1, D10 of 3.86, 3.788 for a load of 16.55 kg obesity and 4.934, 4.393 for an obesity load 19.88 kg and 7.506, 6.718 for an obesity load 29.85 kg compared to other discs of the vertebral column **"Figure 18"**. Finally a normal person (without obesity), Von Mises stresses are concentrated in both discs D1 and D10 with values of 10.974 MPa, 9.858MPa see **"Figure 15"**. In the case where the obesity of load augment that is to say the distance between the load application point and the axis of the spine augment (the most risky cases). These loads will cause according to the maximum distance of major constraints that will generated a phenomenon called disc degeneration (herniated disc) posterior side of the disc from its side will overwrite the spinal nerve (spinal cord) see **"Figure 20"** and **"Figure 21"**.

#### 6. Conclusions

In sum, we concluded for the three cases of anterior load (obese persons) **"Figure 19"**, that the distributions of Von Mises stresses are highest in intervertebral discs and are concentrated in the disk D1, in contact with the L5 vertebra and the sacrum; **"Figure 20"** clearly shows that the level of deformation of Von Mises is maximal in the disc D1, valued at 7.5063 mm / mm. This shows that the distance between the load application point and the axis of the spine has an important role in the increase of solicitation of this one and therefore of its deformation **"Figure 21"**.

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